

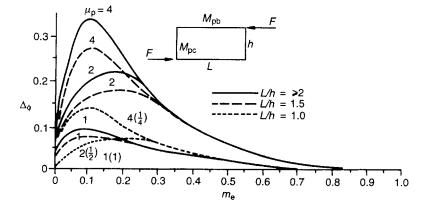
**Fig. 8.12** Plot of  $\delta_{p}$  against  $m_{d}$ . From Wood (1978).

Then the value of the non-dimensional parameterd  $\phi_s$  is calculated using the equation

$$\phi_{\rm s} = 2/(\sqrt{m_{\rm e}} + 1/\sqrt{m_{\rm e}}) \tag{8.17}$$

This parameter was derived for square panels with identical beams and columns, and a correction factor  $\Delta_{\phi}$  must be determined for non-rectangular panels with unequal beams and columns, using Fig. 8.13 in which  $\mu_{\rm p}$  is defined

$$\mu_{\rm p} = \frac{\text{lowest beam plastic moment}}{\text{lowest column plastic moment}}$$
(8.18)



**Fig. 8.13** Design chart for racking loads: optional correction  $\Delta_{\phi}$  added to  $\Phi_{s}$  ( $\mu=M_{pb}/M_{pc}$ ). From Wood (1978).

- If  $\mu_p \ge 1$  (strong beams) use the chart directly.
- If  $\mu_p < 1$  (weak beams) and L/h=1 use  $\mu_p$  value in brackets.
- If  $\mu_p < 1$  (weak beams) and L/h > 1 use  $\mu_p = 1$  curve.

Finally the design strength *F* can be determined using

$$F = (\phi_{\rm s} + \Delta_{\phi}) \left[ 4 \, (\text{smaller } M_{\rm p}) / h \right. \\ \left. + \frac{1}{2} \delta_{\rm p} f_{\rm k} t L / \gamma_{\rm m} \right] / 1.2$$
(8.19)

where the factor 1.2 is an additional factor of safety introduced by Wood for design purposes and  $M_p$  is the effective plastic moment given by  $Z\sigma_y/\gamma_{ms}$ . For design purposes the design strength must be equal to or greater than the design load as shown in Chapter 4.

## (c) Example

Assume the following dimensions and properties:

- Panel height=2m
- Panel length=4m
- Panel thickness=110mm
- Characteristic strength of panel=10N/mm<sup>2</sup>
- Partial safety factor for masonry=3.1
- Section modulus for each column=600 cm<sup>3</sup>
- Section modulus for each beam=800 cm<sup>3</sup>
- Yield stress of steel=250N/mm<sup>2</sup>
- Partial safety factor for steel=1.15
- Effective plastic moment for beam=(800×10<sup>3</sup>)×250/(1.15×10<sup>6</sup>)

- Effective plastic moment for column=130kN/m
- μ<sub>p</sub>=134
- *L/h=*2

These give

$$m_{\rm d} = \frac{8 \times 130 \times 10^6 \times 3.1}{10 \times 110 \times 4^2 \times 10^6} = 0.18$$

From Fig. 8.12,  $\delta_p$ =0.25. So

$$m_{\rm e} = 0.24/0.25 = 0.96$$

$$\phi_{\rm s} = 2/(\sqrt{0.96} + 1/\sqrt{0.96}) = 1.0$$

From Fig. 8.13,  $\Delta_{\phi} = 0$ .